

A Study on the Behavior of Electromagnetic Waves for A Curved Antenna

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Abstract: This paper discuss the potential of a curved electric dipole (of radius $R = r = h$) as a source of electromagnetic waves. We will present the solution of Maxwell equations in one dimension for the antenna. Green functions are employed to solve the toroidal and poloidal modes of the antenna, Simulations are carried out for a frequency range of 0.01 to 10Hz. Results have shown that the antenna is able to detect resistive layers under the sea bed.

Keywords: Electromagnetic wave, Maxwell equation, curve electric dipole

1 Introduction

To detect hydrocarbon beneath the sea bed there many techniques, one of them is the Control source electromagnetic (CSEM). This method employ made electric and magnetic field to excite the earth beneath the sea floor [9], [5], [12] and [16]. In this method, a horizontal electric dipole (HED) ([7]) is used to transmit ultra low frequency (0.1 - 5Hz) electromagnetic waves which is being located approximately 30 - 40m above the seabed to detect resistivity contrasts in the subsurface.

Control Source Electromagnetic (CSEM) theory makes use of the known theory of propagation within medium of varying resistivity contrast. An EM field is prompted into a conductive subsurface and propagated downwards and deep. Spatial distribution of resistivity from the many layers causes the wave behavior and characteristics to be slightly or majorly altered to depict the matter making the subsurface. Marine environment consists of or are made up of highly conductive sediments filled up with salt water. On the other hand some sediments are filled up with more resistive matter such as hydrocarbons and gases. Volcanic rocks and carbonates also represent some of resistive bodies that comprise the subsurface. Resistive constituents of the inhomogeneous subsurface reflect and propagates back to the seafloor some signal which is recorded by receivers equipped with electric and magnetic sensors.

Marine magnetotelluric MT method has been used in the study of the resistivity of seafloor. Among the studies are those conducted in [3], and [6]. They proposed the use of HED controlled-source sounding to study seafloor geology and expanded the concept of marine CSEM to describe a deep-sea experiment. Recent applications of magnetometric resistivity to the marine environment are given in [8], [18], [4],[13], [14], [1] and [2].

Of late, there has been a growing interest in preliminary analysis of MCSEM receiver data through numerical modeling. This has a motive to design optimal SBL survey variables and to obtain insights about the target responses. This work prospects has increased with many applications of the marine CSEM method. ([20], [10], [15], [17] and [11]).

This paper presents a study on the behavior of the electromagnetic waves of a curved antenna whose height (h) equals the radius (r) as a potential antenna in CSEM. In this paper we will introduce the solution of Maxwell equation one dimension for this antenna.. This antenna is located 30 m above the sea bed together with an array of stationery EM receivers for recording the EM waves (see Figure(1)). The solution of Maxwell equation will be in frequency domain. The Green Functions are used to find the solution for the poloidal and toroidal modes (that modes are unique using Helmholtz representation theorem) for the antenna. Numerical solution for the Electric field (magnitude and phase) is obtained using MATLAB software. The effect of frequency and water

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depth on our function (Electric field) for HC detection will be observed.

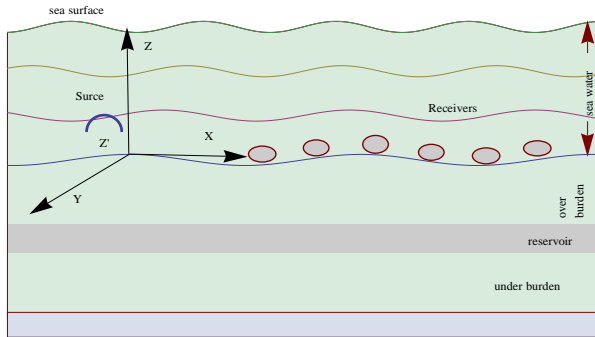


Fig. 1: A design of a basic marine CSEM (SBL) survey model. the height of antenna is $z' = 30$ meters and the height of receivers are zero and the height of water is H . the direction of upward in the direction of z .

2 GOVERNING EQUATION

Consider the diffusion of the fields of a point curved electric dipole in a one dimension layered structure. Given the Maxwell equations:

$$\begin{aligned}\nabla \cdot E &= \frac{Q}{\epsilon_0} \\ \nabla \times E &= -\frac{\partial B}{\partial t} \\ \nabla \cdot B &= 0 \\ \nabla \times B &= \mu(j + \epsilon_0 \frac{\partial E}{\partial t})\end{aligned}\quad (1)$$

where E is the electric field, B is the magnetic field, j is the current density, j_0 is the conduction current, Q is the charge density, ϵ_0 is the electric permittivity, μ_0 is the magnetic permeability, σ is the conductivity of medium, ω is the angular frequency and t is the time. We consider rate of change the charge is zero in our study. Furthermore from Ohms law $J^0 = \sigma E$ (displacement current) so the total current is sum of displacement current and conduction current ($J = -i\omega\epsilon_0 E + J^0$). A low frequency (0.01 to 10 Hz), with resistivity of air and hydrocarbon of (10-11 Ω) and (0.1 to 0.001 Ω) respectively are considered. Hence, the displacement current can be negligible when solving Maxwell's equation in this environment. Then the last equation of Maxwell's equation becomes.

$$\nabla \times B = \mu_0(j^0 + \epsilon_0 \frac{\partial E}{\partial t}) \quad (2)$$

We now define the coordinate system (Cartesian coordinate system), the origin point of this coordinate is on sea surface and the upward is in the positive direction of \hat{z} , and let σ be variation in the direction of \hat{z} only. (See figure 1). The Maxwell equations will be solved in terms of poloidal and toroidal magnetic (PM and TM) modes based on a Helmholtz representation of a vector field. In horizontal planes, The PM mode is marked by electric currents, and the electric field in direction of \hat{z} is zero. But the TM mode is associated with electric currents flowing in planes containing the vertical, and has no vertical magnetic field component.

$$V = \nabla\phi + \nabla \times (\psi\hat{z}) + \nabla \times \nabla \times (\chi\hat{z}) \quad (3)$$

By using Maxwell equation and above equation, the magnetic field can be written as:

$$B = \nabla \times (\Pi\hat{z}) + \nabla \times \nabla \times (\Psi\hat{z}) \quad (4)$$

Where the Π represented to TM mode and Ψ represented to TE mode. The source current density J^0 may be written (toroidal, consoidal and vertical parts) at the form:

$$j^0 = j_z^0\hat{z} + \nabla_h T + \nabla \times (Y\hat{z}) \quad (5)$$

Where T and Y are the scalar functions and j_z^0 is the vertical component of current source. T and Y are satisfy the Poisson equations:

$$\begin{aligned}\nabla_h^2 T &= \nabla_h \cdot j_h^0 \\ \nabla_h^2 Y &= -(\nabla_h \times j_h^0) \cdot \hat{z}\end{aligned}\quad (6)$$

Where ∇_h^2 is the surface Laplacian, ∇_h is the surface gradient and $\nabla_h \times$ surface curl operators.

The electric field can be written as the form:

$$E = \frac{1}{\mu\sigma}(\nabla \times \nabla \times (\Pi\hat{z})) - \frac{1}{\sigma}(j_z^0\hat{z} + \nabla_h T) - i\omega\nabla \times (\Psi\hat{z}) \quad (7)$$

$$B = \hat{z} \times \nabla_h \Pi + \nabla_h \left(\frac{\partial \Psi}{\partial z} \right) - \nabla_h^2 \Psi \hat{z} \quad (8)$$

the scalar functions PM and TM mode satisfy the differential equations:

$$\nabla^2 \Psi - i\omega\mu\sigma\Psi = \mu Y \quad (9)$$

$$\nabla_h^2 \Pi + \sigma \frac{\partial}{\partial z} \left(\frac{\partial \Pi}{\sigma \partial z} \right) - i\omega\mu\sigma\Pi = \mu j_z^0 - \mu\sigma \frac{\partial}{\partial z} \left(\frac{T}{\sigma} \right) \quad (10)$$

From the equations 9 and 10 (diffusion waves) we can show the TM mode is driven by its vertical component and consoidal elements only whereas The PM mode is associated with the toroidal part of the source current. In addition the equations (9 and 10) are parabolic and

hyperbolic diffusion wave equations. At horizontal interfaces The usual boundary conditions must be satisfied on the horizontal components of the electric and magnetic fields. the functions Ψ , $\frac{\partial \Psi}{\partial z}$, Π and $\frac{1}{\mu\sigma} \left(\frac{\partial \Pi}{\partial z} + \mu T \right)$ must be continues. The PM and TM modes in equations (9 and 10) are independent due to the uncoupled of boundary conditions.

3 GREEN FUNCTIONS

Since the Cartesian coordinate is used as the direction of upward in the direction of \hat{z} , and let the east and north be the direction of \hat{x} and \hat{y} respectively. The water column covers the region $-H \leq z \leq 0$ and the conductivity is constant with variation of vertical component $\sigma(-H)$. Let $e^{i\omega t}$ be time dependence. Since all interfaces are planar, so the horizontal Fourier will be convenient to solve the deferential equations (9 and 10) , then the Fourier transform take the form:

$$\tilde{f}(k_x, k_y) = \int_{-\infty}^{\infty} f(x, y) e^{i(k_x x + k_y y)} dx dy \quad (11)$$

$$f(x, y) = \frac{1}{(2\pi)^2} \int_{-\infty}^{\infty} \tilde{f}(k_x, k_y) e^{-i(k_x x + k_y y)} dk_x dk_y \quad (12)$$

where k_x and k_y are wavenumbers for horizontal plan. 2 has given the Green's functions solutions to the Fourier transforms of (9 and 10) for a constant conductivity ocean in the form:

$$G_{\Psi}(z, z') = - \frac{e^{-\beta_0|z-z'|} + R_L^{PM} e^{-\beta_0(z+z'+2H)} + R_U^{PM} e^{\beta_0(z+z')} + R_L^{PM} R_U^{PM} e^{\beta_0(|z-z'|-2H)}}{2\beta_0(1 - R_U^{PM} R_L^{PM} e^{-2\beta_0 H})} \quad (13)$$

$$G_{\pi}(z, z') = - \frac{e^{-\beta_0|z-z'|} + R_L^{TM} e^{-\beta_0(z+z'+2H)} + R_U^{TM} e^{\beta_0(z+z')} + R_L^{TM} R_U^{TM} e^{\beta_0(|z-z'|-2H)}}{2\beta_0(1 - R_U^{TM} R_L^{TM} e^{-2\beta_0 H})} \quad (14)$$

Where $\beta_0^2 = k^2 - i\omega\mu\sigma_0$ (complex) is the ocean diffusion parameter, σ_0 is the electric conductivity of water layer, $k^2 = k_x^2 + k_y^2$ is the magnitude of horizontal wavenumber and R_B^A is the interaction coefficient.

Let the Earth be represented as a stack of N layers of variable with conductivity σ_i and thickness h_i terminated by a half-space that may be insulating, conducting, or a perfect conductor, Chave and Luther (1990) give the stable recursive expressions for the lower diffusion interaction coefficient in the form:

$$R_i^{TM} = \frac{\chi_i + e^{-2\beta_{i+1}h_{i+1}} R_{i+1}^{TM}}{1 + \chi_i e^{-2\beta_{i+1}h_{i+1}} R_{i+1}^{TM}} \quad (15)$$

$$R_i^{PM} = \frac{\alpha_i + e^{-2\beta_{i+1}h_{i+1}} R_{i+1}^{PM}}{1 + \alpha_i e^{-2\beta_{i+1}h_{i+1}} R_{i+1}^{PM}} \quad (16)$$

the coefficients of interface interaction are:

$$\chi_i = \frac{\beta_i \sigma_{i+1} - \beta_{i+1} \sigma_i}{\beta_i \sigma_{i+1} + \beta_{i+1} \sigma_i} \quad (17)$$

$$\alpha_i = \frac{\beta_i - \beta_{i+1}}{\beta_i + \beta_{i+1}} \quad (18)$$

The solutions of (9 and 10) within the ocean at any point for any source function, By using the Green's functions can be written in the form:

$$\tilde{\Psi}(z) = \mu \int_{-H}^0 G_{\Psi}(z, z') \tilde{Y}(z') dz' \quad (19)$$

$$\tilde{\Pi}(z') = \mu \int_{-H}^0 \left(G_{\pi}(z, z') \tilde{j}_z^0(z') - G_{\Psi}(z, z') \sigma \frac{\partial}{\partial z'} \left(\frac{\tilde{T}(z')}{\sigma} \right) \right) dz' \quad (20)$$

The Solutions for the EM fields are obtained using the inverse Fourier transforms (11) and calculation of the horizontal and vertical derivatives.

4 NEW ANTENNA DESIGN

Consider a curved electric dipole antenna with height (h) equals radius (r), hence in our case $R = r = h$. The centre of curved antenna is concede to the point $(0, 0, z')$ and the orientation of it in xz plane and the axes y is orthogonal to the plane as shown in Figure 2.

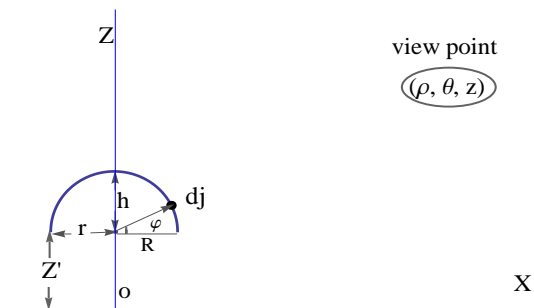


Fig. 2: Diagram showing the geometry for curved electric dipole antenna with $h = r$ and radius R . The dipole source lies in the xz plane (y Axes is orthogonal on the page) at the point $(0, 0, z')$ with current flowing. the oriented of current in direction of anticlockwise. The view point point at (ρ, θ, z) is depicted by ellipse

Assume infinitesimal piece of curved antenna oriented at a anticlockwise angle φ carries the electric current density, So the infinitesimal current density can be written in the form:

$$dj^0 = IR\delta(x - R \cos \varphi) \delta(y) \delta(z - z' + R \sin \varphi) d\varphi \hat{\phi} \quad (21)$$

where I is the electric dipole current and $\hat{\varphi}$ is the unit vector in the direction of φ that is equal to $(-\sin\varphi\hat{x} - \cos\varphi\hat{z})$, so by integral of equation (21) over semi circle ($\varphi = 0 \rightarrow \pi$), so the source current density can be written as the form:

$$j^0(\rho, z) = -IR\delta(y)$$

$$\int_0^\pi \delta(x - R\cos\varphi)\delta(z - z' + R\sin\varphi)(\sin\varphi\hat{x} + \cos\varphi\hat{z})d\varphi \quad (22)$$

From equations (5,6) by taking Fourier transform of them and using equation (22) we can find:

$$\tilde{T} = -\frac{ik_x IR}{k^2} \int_0^\pi e^{ik_x R\cos\varphi} \delta(z - z' + R\sin\varphi) \sin\varphi d\varphi \quad (23)$$

$$\tilde{Y} = \frac{ik_y IR}{k^2} \int_0^\pi e^{ik_x R\cos\varphi} \delta(z - z' + R\sin\varphi) \sin\varphi d\varphi \quad (24)$$

$$\tilde{j}_z^0 = -IR \int_0^\pi e^{ik_x R\cos\varphi} \delta(z - z' + R\sin\varphi) \cos\varphi d\varphi \quad (25)$$

By substituting into equations (19 and 20) and taking inverse Fourier transform and using the Poisson's formula:

$$\int_0^{2\pi} e^{\pm ik\zeta \cos(\theta - \vartheta)} d\theta = 2\pi J_0(k\zeta) \quad (26)$$

where $J_0(k\zeta)$ is the first kind of Bessel function with order 0 and ϑ an arbitrary angle and $\zeta^2 = \rho^2 + R^2 \cos^2\varphi - 2\rho R \cos\varphi \cos\theta$, $\rho^2 = x^2 + y^2$. We can find:

$$\Psi(\rho, z) = -\frac{\mu IR}{2\pi} \int_0^\infty \int_0^\pi \frac{h_\Psi(z, z' - R\sin\varphi)}{k} \frac{\partial J_0(k\zeta)}{\partial y} \sin\varphi d\varphi dk \quad (27)$$

and $\Pi(\rho, z) =$

$$\frac{\mu IR}{2\pi} \int_0^\infty \int_0^\pi \left(-\frac{h_\Psi(z, z' - R\sin\varphi)}{k} J_0(k\zeta) \cos\varphi + \frac{\partial h_\pi(z, z' - R\sin\varphi)}{\partial z'} \frac{\partial J_0(k\zeta)}{k\partial x} \sin\varphi \right) d\varphi dk \quad (28)$$

Where $h_\Psi = G_\Psi - G_\Psi^0$ and $\frac{\partial h_\pi}{\partial z'} = \frac{\partial G_\pi}{\partial z'} - \frac{\partial G_\pi^0}{\partial z'}$ where the superscript 0 refers to the Greens function with $k = 0$. So from equation 7 and using equations 27 and 28 we can write the electric field wave equation in Cartesian coordinate in the form:

$$E_x(\rho, z) = i\omega a \int_0^\infty \left(\left(kJ_0(k\rho) \sin^2\theta + \frac{J_1(k\rho)}{\rho} \cos 2\theta \right) \frac{\partial h_\Psi}{\partial z'} + \left(-kJ_0(k\rho) \cos^2\theta + \frac{J_1(k\rho)}{\rho} \cos 2\theta \right) \frac{\partial h_\pi}{\partial z} \right) dk \quad (29)$$

$$E_y(\rho, z) = i\omega a \sin\theta \cos\theta \int_0^\infty kJ_2(k\rho) \left(\frac{\partial h_\Psi}{\partial z'} + \frac{\partial h_\pi}{\partial z} \right) dk \quad (30)$$

$$E_z(\rho, z) = i\omega a \cos\theta \int_0^\infty k^2 J_1(k\rho) G_\pi dk \quad (31)$$

where J_1, J_2 is the Bessel functions of first kind with the order 1, 2 respectively, and θ is the azimuth. where in our study the inline axis in the direction of x axis see figure 2.

By using equation(8) we can find the Magnetic field in cartesian coordinate in the forms:

$$B_x(\rho, z) = a \sin\theta \cos\theta \int_0^\infty kJ_2(k\rho) \left(\frac{\partial^2 h_\Psi}{\partial z \partial z'} - h_\pi \right) dk \quad (32)$$

$$B_y(\rho, z) = a$$

$$b \int_0^\infty \left(-kJ_0(k\rho) \cos^2\theta + \frac{J_1(k\rho)}{\rho} \cos 2\theta \right) h_\pi dk - \int_0^\infty \left(kJ_0(k\rho) \sin^2\theta + \frac{J_1(k\rho)}{\rho} \cos 2\theta \right) \frac{\partial^2 h_\Psi}{\partial z \partial z'} dk \quad (33)$$

$$B_z(\rho, z) = a \sin\theta \int_0^\infty k^2 J_1(k\rho) \left(\frac{\partial G_\Psi}{\partial z'} \right) dk \quad (34)$$

5 NUMERICAL SOLUTION

Now we will give the numerical solution of electric field. The electric field equations in the directions of x and y are depending on TM and PM mode while electric field in the direction of z depends on TM only. The receivers read the data that comes from the source, interaction with sea surface and interaction with oil, and some parts where there is interaction with sea surface and oil at the same time. (Equations 12 and 13). MATLAB software is used to solve the equations (28, 29 and 30) to determine the behaviour of electromagnetic fields and Gauss-Kronrod quadrature method is used for finding the integration. These equations will be solved based on the geological model in Figure 3.

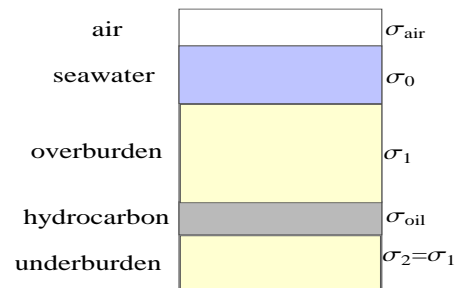


Fig. 3: sketch design for our problem

In our solution, we let the conductivity of air be $\sigma_{air} = 10^{-11} s/m$, water $\sigma_0 = 4 s/m$, overburden and underburden $\sigma_1 = \sigma_2 = 1.5 s/m$ and oil $\sigma_{oil} = 0.001 s/m$. the magnetic permeability are equal for all variable ($4\pi \times 10^{-7} NA^{-2}$) except for water is $0.999991 \times 4\pi \times 10^{-7} NA^{-2}$. In our model the height of source is 30m and the receivers are butting on sea floor $z = 0$. the direction of x is the inline direction while the direction of broadside is any direction has an angel (azimuth) with x axis (inline) see figure (2). The curve antenna has $r = h = R = 85.9437m$ and the length of its arc equal to 270m.

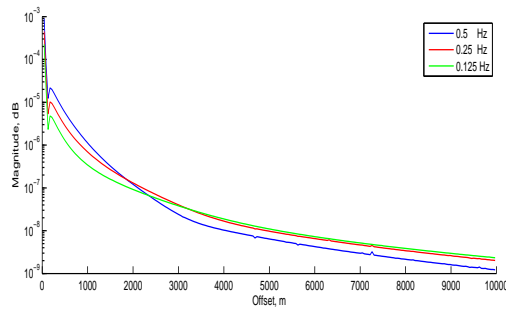


Fig. 4: magnitude of electric field (Ex) versus offset. the frequencies are 0.5, 0.25, 0.125Hz and the height of seawater is 500 m and overburden is 1000 m and the thickness of hydrocarbon layer is 100 m. with 0° Azimuth

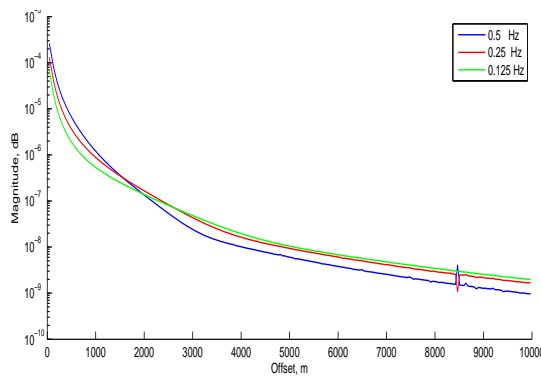


Fig. 5: magnitude of electric field (Ey) versus offset. the frequencies are 0.5, 0.25, 0.125Hz and the height of seawater is 500 m and overburden is 1000 m and the thickness of hydrocarbon layer is 100 m. with 45° Azimuth

Figures 4- 6 shows the magnitude of the electric field with varying frequencies and azimuth. The frequencies considered in the simulations are 0.5Hz, 0.25Hz and

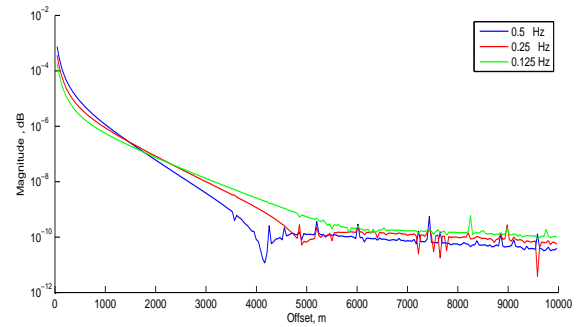


Fig. 6: magnitude of electric field (Ez) versus offset. the frequencies are 0.5, 0.25, 0.125Hz and the height of seawater is 500 m and overburden is 1000 m and the thickness of hydrocarbon layer is 100 m. with 45° Azimuth

0.125Hz. The simulation results shows that the magnitude of electric field is high(put the approximate values of the E-field) even at offsets greater than 5km. The results also show that the highest electric field magnitude is at a frequency of 0.125Hz for all directions (x,y and z axis) which implies that the curve antenna is able to operate well even at low frequency. This result implies the potential of the new antenna in CSEM since this method makes use of low frequency.

Simulations are also carried out to see the behavior of the E-fields when the sea water depth is varied from 200m (shallow water) to 1500m (deep water). A frequency of 0.125Hz, overburden of 1000 m and hydrocarbon thickness of 100 m are considered in the simulation. Results are shown in Figures 7, 8, 9, 10, 11 and 12.

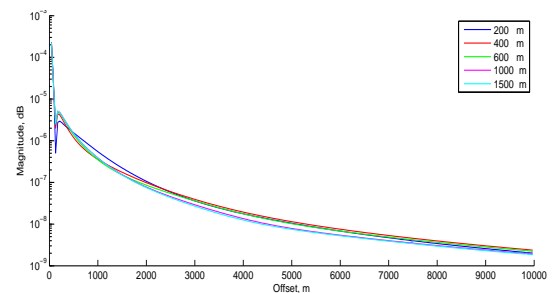


Fig. 7: . Magnitude of electric field (Ex) versus offset (using log scale for y axis). the height of seawater is 200, 400, 600, 1000, 1500 m and overburden is 1000 m and the thickness of hydrocarbon layer is 100 m. and the frequency is 0.125H. with 0° Azimuth

The Electric field values along Ex component is higher at the near offset and are large for shallow water

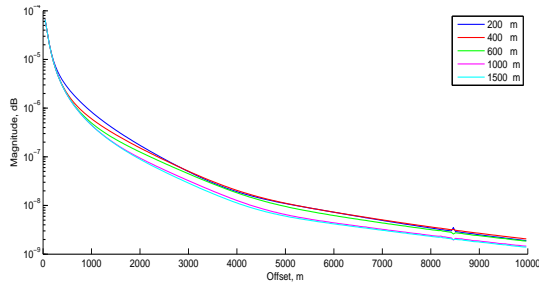


Fig. 8: . Magnitude of electric field (E_y) versus offset (using log scale for y axis). the height of seawater is 200, 400, 600, 1000, 1500 m and overburden is 1000 m and the thickness of hydrocarbon layer is 100 m. and the frequency is 0.125H. with 45° Azimuth

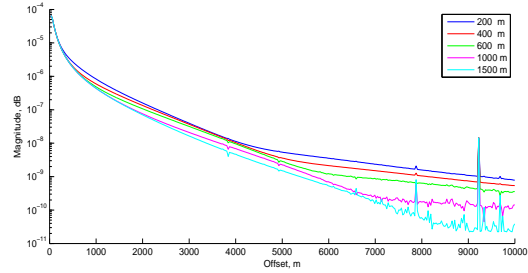


Fig. 11: . Magnitude of electric field (E_y) versus offset (using log scale for y axis). the height of seawater is 200, 400, 600, 1000, 1500 m and overburden is 1000 m, without hydrocarbon layer and the frequency is 0.125H. with 45° Azimuth

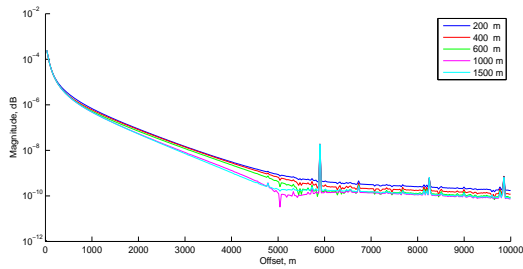


Fig. 9: . Magnitude of electric field (E_z) versus offset (using log scale for y axis). the height of seawater is 200, 400, 600, 1000, 1500 m and overburden is 1000 m and the thickness of hydrocarbon layer is 100 m. and the frequency is 0.125H. with 0° Azimuth

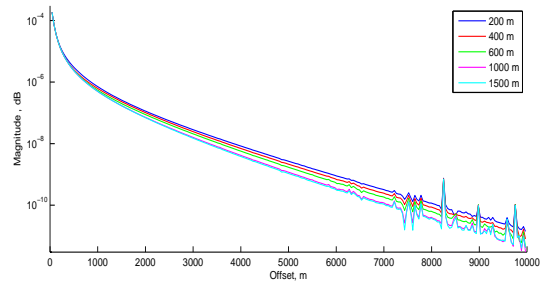


Fig. 12: Magnitude of electric field (E_z) versus offset (using log scale for y axis). the height of seawater is 200, 400, 600, 1000, 1500 m and overburden is 1000 m, without hydrocarbon layer. and the frequency is 0.125H. with 0° Azimuth

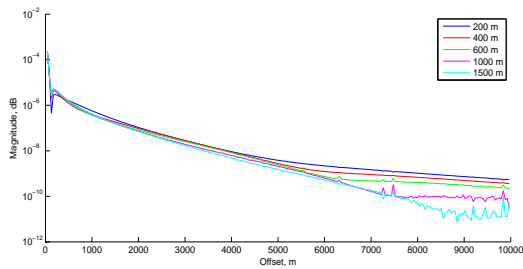


Fig. 10: . Magnitude of electric field (E_x) versus offset (using log scale for y axis). the height of seawater is 200, 400, 600, 1000, 1500 m and overburden is 1000 m, without hydrocarbon layer and the frequency is 0.125H. with 0° Azimuth

but big for shallow water environment.

Now we give the behavior of electric field for variation of overburden. The frequency is 0.125Hz, the height of sea water is 500m and the thickness of hydrocarbon is 100 m.

From the Figures 13, 14 and 15 it is clear that the magnitude of electric field is big for shallow overburden and vice versa. The reason is that, the electric field wave will decay faster when the thickness of the overburden increases. These results have shown that the new antenna is able to detect the different resistive layers just like the current horizontal antenna.

environment Also, the E-field along the E_y component decreases as the offset increases. As E_z is the vertical component, the magnitude of E_z is small for deep water

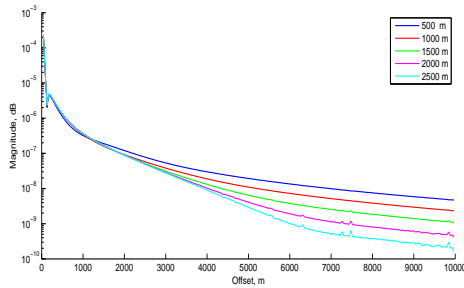


Fig. 13: Magnitude of electric field (E_x) versus offset (using log scale for y axis). the height of seawater is 500 m and overburdens are 500, 1000, 1500, 2000, 2500 m and the thickness of hydrocarbon layer is 100 m. and the frequency is $0.125H$. with 0° Azimuth

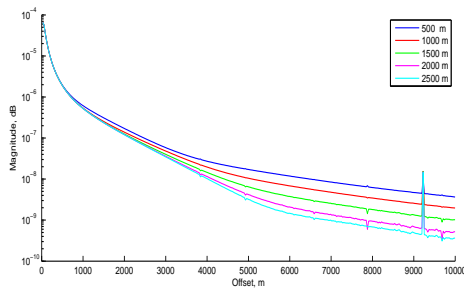


Fig. 14: Magnitude of electric field (E_y) versus offset (using log scale for y axis). the height of seawater is 500 m and overburdens are 500, 1000, 1500, 2000, 2500 m and the frequency is $0.125H$. with 45° Azimuth

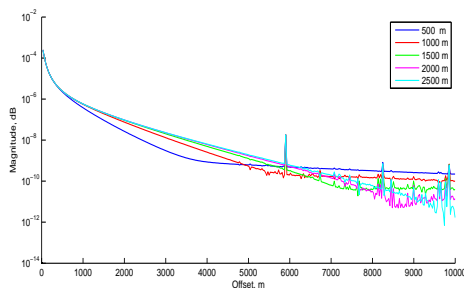


Fig. 15: Magnitude of electric field (E_z) versus offset (using log scale for y axis). the height of seawater is 500 m and overburdens are 500, 1000, 1500, 2000, 2500 m and the frequency is $0.125H$. with 0° Azimuth

6 CONCLUSION

This paper introduces the solution of Maxwell Equation in one dimension using a new design of antenna with $h = r$. It has been shown the new antenna is able to detect the resistivity contrast in homogenous layers media. It is

observed that smaller frequencies are better in detecting the resistive layers. Difference in the Electric field is also observed in the presence of hydrocarbon. These simulations seem to indicate that this antenna has the potential to be used as a source of EM waves.

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