

# The Pitch, the Angle of Pitch, and the Distribution Parameter of a Closed Ruled Surface

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**Abstract:** In this paper, the pitch, the angle of pitch, and the distribution parameter of the closed ruled surfaces, generated by tangent, bi-normal, normal vectors, and unit Darboux vector of a unit dual spherical motion, are studied on the Frenet frame.

**Keywords:** Dual Steiner vector, dual spherical motion, pitch of the motion, Pfaffian vector, ruled surface.

## 1 Introduction

For the analysis of spatial motions in differential geometry [2, 6] and in kinematics of the spatial mechanisms [11–13], the use of dual vectors, dual quaternion, and dual matrix algebra over the ring of dual numbers is a very direct method. Important properties of a real vector analysis of real matrix algebra are valid for the dual vectors and dual matrices. The principal part of this method is based on work by E. Study [12]. The essential idea is to replace points by straight lines as fundamental building blocks of geometric structure. The set of oriented lines in Euclidean three-dimensional space  $E^3$  is in one-to-one correspondence with the points of a unit dual sphere in the dual space  $D^3$  of triples of dual numbers.

The definition of the Steiner vector for the real unit sphere [1] is extended [2] to the definition of dual Steiner vector. In [2], an expression of the pitch of a closed ruled surface is derived in terms of the elements of the dual Steiner vector. Using this expression, the spatial extensions for planar [2] and spherical [1, 4] theorems called Steiner theorems and Holditch theorems are given.

The motion corresponding to the dual spherical closed motion  $K/K'$  on  $D$ -module is the one-parameter motion  $H/H'$  on the line-space. The closed ruled surface  $(X)$ , which is drawn by the line  $\vec{X}$  of  $H$  on the fixed space  $H'$ , the pitch, and the angle of pitch of the closed ruled surface  $(X)$  are studied in [3].

In this paper, the pitch, the angle of pitch, and distribution parameter of the closed ruled surface each of which generated by tangent, bi-normal, normal vectors, and unit Darboux vector on unit dual sphere, respectively, are investigated.

## 2 The Pitch of a Closed Ruled Surface

Let  $H'$  and  $H$  denote the fixed and moving line-spaces, respectively. According to the result of E. Study, unit dual spheres  $K'$  and  $K$  centered at a point  $M$  correspond to these spaces on  $D$ -module, respectively. Also, dual-spherical motion  $K/K'$  corresponds to one-parameter spatial motion  $H/H'$ . Let us take a line  $\vec{X}$  on  $H$ . That is to say, we consider a fixed point  $X$  of the unit dual sphere  $K$ . During the motion  $H/H'$ , the line  $\vec{X}$  traces a ruled surface  $(X)$  which is called the orbit surface on  $H'$ . The variation of the point  $X$  according to the fixed sphere  $K'$ , i.e., the variation of the line  $\vec{X}$  on  $H'$  is

$$d_f \vec{X} = \vec{\Psi} \wedge \vec{X},$$

where the vector  $\vec{\Psi} = \vec{\psi} + \varepsilon \vec{\psi}^* = (\Psi_1, \Psi_2, \Psi_3)$  with  $\Psi_i = \psi_i + \varepsilon \psi_i^*$ ,  $i = 1, 2, 3$ , is called the instantaneous Pfaffian vector of the motion  $H/H'$ .

The ruled surface  $(X)$  is given by  $\vec{X} = \vec{X}(t) = \vec{x}(t) + \varepsilon \vec{x}^*(t)$ , where  $\vec{X} = \vec{X}(t)$  is the unit dual vectorial function

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parameterized by  $t \in \mathbb{R}$ . The dual curve  $(X)$  is the dual spherical formation of the ruled surface. For the dual arc element  $d\Phi = d\varphi + \varepsilon d\varphi^*$  on the dual spherical curve  $\vec{X} = \vec{X}(t)$ ,

$$d\Phi^2 = \langle d\vec{X}, d\vec{X} \rangle = \langle d\vec{x}, d\vec{x} \rangle + 2\varepsilon \langle d\vec{x}, dx^* \rangle$$

is valid. The distribution parameter of the ruled surface is defined [5] by

$$\frac{1}{d} = \frac{\langle d\vec{x}, d\vec{x} \rangle}{\langle d\vec{x}, dx^* \rangle} = \frac{d\varphi \cdot d\varphi^*}{d\varphi^2} = \frac{d\varphi^*}{d\varphi}.$$

**Definition 1.** Let  $K$  be the moving unit dual sphere. Subject to the condition that the pitch of the motion is nonvanishing, a new coordinate system is introduced by  $\{\vec{R}_1, \vec{R}_2, \vec{P} = \vec{R}_3\}$ . This frame is called a canonical coordinate frame. For this case,  $\vec{\Psi} = \Psi_3 \vec{R}_3 = \Psi_3 \vec{P}$  is the instantaneous Pfaffian vector [5].

The declaration of the variation of a point of  $X \in K$  according to the canonical coordinate frame on one-parameter motion  $K/K'$  is given [5] by

$$\begin{aligned} d_f \vec{X} &= \vec{\Psi} \wedge \vec{X} = \Psi_3 (\vec{P} \wedge \vec{X}) \\ &= \Psi_3 (\vec{R}_3 \wedge \vec{X}) = \Psi_3 (X_1 \vec{R}_2 - X_2 \vec{R}_1), \end{aligned}$$

where  $\vec{\Psi} = \Psi_3 \vec{R}_3$ ,  $\Psi_3 = \Psi_3 + \varepsilon \Psi_3^*$ ,  $\vec{X} = X_1 \vec{R}_1 + X_2 \vec{R}_2 + X_3 \vec{R}_3$ , and  $X_i = x_i + \varepsilon x_i^*$ ,  $i = 1, 2, 3$ . The distribution parameter of the ruled surface is

$$\frac{1}{d} = p - \frac{x_2 x_3^*}{1 - x_3^2},$$

where  $p = \frac{\Psi_3^*}{\Psi_3}$  is the pitch [5] of the motion  $H/H'$ .

### 3 The Distribution Parameter of a Closed Ruled Surface

On the one-parameter dual spherical motion, the fixed point  $X \in K$  constructs a dual curve on  $K'$ . The tangent, bi-normal, and normal of the dual curve  $(X)$  at a point  $X$  are

$$\vec{T} = \frac{d_f \vec{X}}{\|d_f \vec{X}\|} = \frac{\vec{\Psi} \wedge \vec{X}}{\|\vec{\Psi} \wedge \vec{X}\|},$$

$$\vec{B} = \frac{d_f \vec{X} \wedge d_f^2 \vec{X}}{\|d_f \vec{X} \wedge d_f^2 \vec{X}\|},$$

$$\vec{N} = \vec{B} \wedge \vec{T},$$

respectively.

**Theorem 1.** On the one-parameter dual motion  $K/K'$ , the tangent, bi-normal, and normal vectors of a dual curve  $(X)$  at a point  $X$  are given by

$$\vec{T} = \frac{1}{\sqrt{1 - X_3^2}} (-X_2 \vec{R}_1 + X_1 \vec{R}_2),$$

$$\vec{N} = \frac{-1}{\sqrt{1 - X_3^2}} (X_1 \vec{R}_1 + X_2 \vec{R}_2),$$

$$\vec{B} = \vec{R}_3,$$

respectively, where  $X = (X_1, X_2, X_3)$ .

*Proof.* Suppose that  $R = \begin{pmatrix} \vec{R}_1 \\ \vec{R}_2 \\ \vec{R}_3 \end{pmatrix}$ , where  $\{\vec{R}_1, \vec{R}_2, \vec{R}_3\}$  is

a unit dual orthogonal frame for 3-space  $D^3$ . Since  $X$  is on the unit dual sphere  $K$ , we may write that

$$\vec{X} = X_1 \vec{R}_1 + X_2 \vec{R}_2 + X_3 \vec{R}_3 = X^T R,$$

$$\|\vec{X}\|^2 = X_1^2 + X_2^2 + X_3^2 = \mathbf{1} = (1, 0),$$

where  $X = \begin{pmatrix} X_1 \\ X_2 \\ X_3 \end{pmatrix}$ , and  $\vec{X}$  is the dual vector corresponding

to  $X$ . The displacements of  $R$  with respect to  $K$  and  $K'$ , the dual moving, and fixed sphere, respectively, are given by

$$dR = \Omega R, \quad d'R = \Omega' R,$$

$$\Omega = \begin{pmatrix} 0 & \Omega_3 & -\Omega_2 \\ -\Omega_3 & 0 & \Omega_1 \\ \Omega_2 & -\Omega_1 & 0 \end{pmatrix}$$

and

$$\Omega' = \begin{pmatrix} 0 & \Omega'_3 & -\Omega'_2 \\ -\Omega'_3 & 0 & \Omega'_1 \\ \Omega'_2 & -\Omega'_1 & 0 \end{pmatrix}.$$

Then the displacements of  $\vec{X}$  with respect to  $K$  and  $K'$  are given by

$$d\vec{X} = dX^T R + X^T dR = (dX^T + X^T \Omega) R \quad (1)$$

and

$$d'\vec{X} = d'^T R + X^T d'R = (d'^T + X^T \Omega') R, \quad (2)$$

respectively. Since  $\Omega$  and  $\Omega'$  are anti-symmetric matrixes, we have

$$\Omega^T = -\Omega, \quad \Omega'^T = -\Omega'.$$

For any fixed vector  $\vec{X}$ , we get

$$d\vec{X} = 0, \quad d'\vec{X} = 0.$$

Therefore from equations (1) and (2), we get

$$\begin{aligned} dX^T + X^T \Omega &= 0, \\ dX^T &= -X^T \Omega = X^T \Omega^T \end{aligned} \quad (3)$$

and

$$\begin{aligned} d'X^T + X^T \Omega' &= 0, \\ d'X^T &= -X^T \Omega' = X^T \Omega'^T. \end{aligned} \tag{4}$$

Now, suppose that  $X$  is fixed in  $K$  and let us calculate its velocity  $d_f X$  with respect to  $K'$ . Then we obtain that

$$\begin{aligned} d_f \vec{X} &= d' \vec{X} - d \vec{X} \\ &= X^T (\Omega' - \Omega) R. \end{aligned}$$

If we define a new dual vector whose components in the relative system are  $\Psi_i = \Omega'_i - \Omega_i$ , where  $i = 1, 2, 3$ , and

$$\begin{aligned} \vec{\Psi} &= (\Psi_1, \Psi_2, \Psi_3) \\ &= \Psi_1 \vec{R}_1 + \Psi_2 \vec{R}_2 + \Psi_3 \vec{R}_3, \end{aligned}$$

then we get

$$d_f \vec{X} = \vec{\Psi} \wedge \vec{X}, \tag{5}$$

where  $\vec{\Psi}$  is the Pfaffian vector corresponding to the dual spherical motion  $K/K'$ . To calculate the acceleration  $J = d_f^2 \vec{X}$  of  $X$ , we have

$$\begin{aligned} J &= d_f^2 \vec{X} = \vec{\Psi} \wedge (\vec{\Psi} \wedge \vec{X}) + \vec{\Psi} \wedge \vec{X} \\ &= -\langle \vec{\Psi}, \vec{\Psi} \rangle \vec{X} + \langle \vec{\Psi}, \vec{X} \rangle \vec{\Psi} + \vec{\Psi} \wedge \vec{X} \\ &= -\|\vec{\Psi}\|^2 \vec{X} + \langle \vec{\Psi}, \vec{X} \rangle \vec{\Psi} + \vec{\Psi} \wedge \vec{X} \\ &= -\Psi^2 \vec{X} + \langle \vec{\Psi}, \vec{X} \rangle \vec{\Psi} + \vec{\Psi} \wedge \vec{X}. \end{aligned}$$

By using the matrix form, the relations (3) and (4) yield

$$d_f X = MX$$

and

$$J = d_f^2 X = (M^2 + \dot{M})X,$$

where

$$M = \begin{pmatrix} 0 & -\Psi_3 & \Psi_2 \\ \Psi_3 & 0 & -\Psi_1 \\ -\Psi_2 & \Psi_1 & 0 \end{pmatrix}$$

and

$$\dot{M} = dM = \begin{pmatrix} 0 & -\dot{\Psi}_3 & \dot{\Psi}_2 \\ \dot{\Psi}_3 & 0 & -\dot{\Psi}_1 \\ -\dot{\Psi}_2 & \dot{\Psi}_1 & 0 \end{pmatrix}.$$

Hence we obtain

$$\begin{aligned} M^2 &= \begin{pmatrix} -\Psi_3^2 - \Psi_2^2 & \Psi_1 \Psi_2 & \Psi_1 \Psi_3 \\ \Psi_1 \Psi_2 & -\Psi_3^2 - \Psi_1^2 & \Psi_2 \Psi_3 \\ \Psi_1 \Psi_3 & \Psi_2 \Psi_3 & -\Psi_2^2 - \Psi_1^2 \end{pmatrix} \\ &= \begin{pmatrix} -\Psi^2 - \Psi_1^2 & \Psi_1 \Psi_2 & \Psi_1 \Psi_3 \\ \Psi_1 \Psi_2 & \Psi^2 + \Psi_2^2 & \Psi_2 \Psi_3 \\ \Psi_1 \Psi_3 & \Psi_2 \Psi_3 & -\Psi^2 - \Psi_3^2 \end{pmatrix}. \end{aligned}$$

If  $\vec{\Psi} = \Psi_3 \vec{R}_3$ , then  $\Psi_1 = \Psi_2 = 0$ . Thus,

$$M = \begin{pmatrix} 0 & -\Psi_3 & 0 \\ \Psi_3 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix},$$

and hence the velocity vector of  $X \in K$  is given by

$$\begin{aligned} d_f \vec{X} &= MX = \begin{pmatrix} -\Psi_3 X_2 \\ \Psi_3 X_1 \\ 0 \end{pmatrix} \\ &= \Psi_3 (-X_2 \vec{R}_1 + X_1 \vec{R}_2) \end{aligned}$$

and

$$\begin{aligned} \vec{T} &= \frac{d_f \vec{X}}{\|d_f \vec{X}\|} \\ &= \frac{\Psi_3 (-X_2 \vec{R}_1 + X_1 \vec{R}_2)}{\sqrt{\Psi_3^2 (X_2^2 + X_1^2)}} \\ &= \frac{-1}{\sqrt{1 - X_3^2}} (X_2 \vec{R}_1 - X_1 \vec{R}_2). \end{aligned}$$

By using the same arguments, it is easy to see that  $\vec{B} = \vec{R}_3$ . Therefore

$$\begin{aligned} \vec{N} &= \vec{B} \wedge \vec{T} = \vec{R}_3 \wedge \frac{-1}{\sqrt{1 - X_3^2}} (X_2 \vec{R}_1 - X_1 \vec{R}_2) \\ &= \frac{-1}{\sqrt{1 - X_3^2}} (X_2 \vec{R}_3 \wedge \vec{R}_1 - X_1 \vec{R}_3 \wedge \vec{R}_2) \\ &= \frac{-1}{\sqrt{1 - X_3^2}} (X_2 \vec{R}_2 + X_1 \vec{R}_1). \end{aligned}$$

This completes the proof.

From Theorem 1, the following corollary can be obtained.

**Corollary 1.** On the one-parameter motion  $K/K'$ , the unit Darboux vector is

$$\begin{aligned} \vec{D}_0 &= \frac{\tau \vec{T} + \kappa \vec{B}}{\sqrt{\tau^2 + \kappa^2}} \\ &= \frac{1}{\sqrt{\tau^2 + \kappa^2}} \left[ \frac{\tau}{\sqrt{1 - X_3^2}} (-X_2 \vec{R}_1 + X_1 \vec{R}_2) + \kappa \vec{R}_3 \right], \end{aligned}$$

where  $\kappa = k_1 + \varepsilon k_1^*$  and  $\tau = k_2 + \varepsilon k_2^*$  are the first and second dual curvatures, respectively, and  $\vec{X} = (X_1, X_2, X_3)$ .

**Theorem 2.** Consider a point  $T$  on the unit moving dual sphere  $K$  of the dual-spherical motion  $K/K'$ , corresponding to one-parameter spatial motion  $H/H'$ ,

such that during the motion  $H/H'$ , the line  $\vec{T}$  draws a ruled surface ( $T$ ) on the fixed space  $H'$ . Then the distribution parameter of this ruled surface is

$$\left(\frac{1}{d}\right)_T = p = \frac{\Psi_3^*}{\Psi_3}.$$

*Proof.* The declaration of the variation of a point  $T$  according to the canonical coordinate frame of the one-parameter motion  $K/K'$  is

$$\begin{aligned} d_f \vec{T} &= \vec{\Psi} \wedge \vec{T} = \Psi_3 (\vec{R}_3 \wedge \vec{T}) \\ &= \frac{-\Psi_3}{\sqrt{1-X_3^2}} (X_2 \vec{R}_1 + X_1 \vec{R}_2). \end{aligned}$$

The distribution parameter of the ruled surface is

$$\left(\frac{1}{d}\right)_T = \frac{d\Phi \cdot d\Phi^*}{d\Phi^2} = \frac{\Psi_3^* \cdot \Psi_3}{\Psi_3^2} = \frac{\Psi_3^*}{\Psi_3} = p,$$

where  $d\Phi = d\varphi + \varepsilon d\varphi^*$  denotes the dual arc element of the ruled surface ( $T$ ).

**Theorem 3.** Consider a point  $B$  on the unit moving dual sphere  $K$  such that during the motion  $H/H'$ , the line  $\vec{B}$  draws a ruled surface ( $B$ ) on the fixed space  $H'$ . Then the distribution parameter of this ruled surface is undefined.

*Proof.* The declaration of the variation of the point  $B$  according to the canonical coordinate frame on the one-parameter motion  $K/K'$  is

$$d_f \vec{B} = \vec{\Psi} \wedge \vec{B} = \Psi_3 (\vec{R}_3 \wedge \vec{B}) = 0,$$

since  $\vec{B} = \vec{R}_3$ . So on the motion  $K/K'$ , the point  $B$  is fixed and the distribution parameter of the ruled surface is undefined.

**Theorem 4.** Consider a point  $N$  on the unit moving dual sphere  $K$  such that during the motion  $H/H'$ , the line  $\vec{N}$  draws a ruled surface ( $N$ ) on the fixed space  $H'$ . Then the distribution parameter of this ruled surface is

$$\left(\frac{1}{d}\right)_N = \frac{\Psi_3^*}{\Psi_3} = p.$$

*Proof.* The declaration of the variation of the point  $N$  according to the canonical coordinate frame on the one-parameter motion  $K/K'$  is

$$d_f \vec{N} = \vec{\Psi} \wedge \vec{N} = \Psi_3 (\vec{R}_3 \wedge \vec{N}) = \frac{\Psi_3}{\sqrt{1-X_3^2}} (X_2 \vec{R}_1 - X_1 \vec{R}_2).$$

The distribution parameter of the ruled surface is

$$\left(\frac{1}{d}\right)_N = \frac{\Psi_3^*}{\Psi_3} = p,$$

where  $d\Phi = d\varphi + \varepsilon d\varphi^*$  is the dual arc element of the ruled surface ( $N$ ) and  $p$  is the pitch of the motion.

**Theorem 5.** Consider a point  $D_0$  on the unit moving dual sphere  $K$  such that during the motion  $H/H'$ , the line  $\vec{D}_0$  draws a ruled surface ( $D_0$ ) on the fixed space  $H'$ . Then the distribution parameter of this ruled surface is

$$\left(\frac{1}{d}\right)_{D_0} = \frac{k_1 k_1^* + k_2 k_2^*}{k_1^2 + k_2^2} + \frac{k_2^*}{k_2} + p,$$

where  $p$  is the pitch of the motion and  $k_1, k_2$  are the first and second dual curvatures, respectively.

*Proof.* The declaration of the variation of the point  $D_0$  according to the canonical coordinate frame on the one-parameter motion  $K/K'$  is

$$d_f \vec{D}_0 = \vec{\Psi} \wedge \vec{D}_0 = \frac{-\tau \Psi_3}{\sqrt{\tau^2 + k^2} \sqrt{1-X_3^2}} (X_1 \vec{R}_1 + X_2 \vec{R}_2).$$

The distribution parameter of the ruled surface is

$$\left(\frac{1}{d}\right)_{D_0} = \frac{k_1 k_1^* + k_2 k_2^*}{k_1^2 + k_2^2} + \frac{k_2^*}{k_2} + p,$$

where  $d\Phi = d\varphi + \varepsilon d\varphi^*$  is the dual arc element of the ruled surface ( $D_0$ ).

## 4 The Pitch and the Angle of Pitch

There are four cases of the pitch and angle of pitch of the closed ruled surfaces ( $T$ ), ( $N$ ), ( $B$ ), and ( $D_0$ ) on the canonical coordinate frame.

**Theorem 6.** The pitch, the angle of pitch, and the dual angle of pitch of the closed ruled surface ( $T$ ) on the canonical coordinate frame are vanishing.

*Proof.* We know that

$$\vec{T} = \frac{1}{\sqrt{1-X_3^2}} (-X_2 \vec{R}_1 + X_1 \vec{R}_2)$$

is valid, where  $\vec{T} = \vec{t} + \varepsilon \vec{t}^*$  and  $X_i = \vec{x}_i + \varepsilon \vec{x}_i^*$ ,  $\vec{R}_i = \vec{r}_i + \varepsilon \vec{r}_i^*$  for  $i = 1, 2, 3$ , and

$$\vec{t} = \frac{1}{\sqrt{1-x_3^2}} (-x_2 \vec{r}_1 + x_1 \vec{r}_2),$$

$$\vec{t}^* = \frac{1}{\sqrt{1-x_3^2}} (\lambda_1 \vec{r}_1 + \lambda_2 \vec{r}_2 - x_2 \vec{r}_1^* + x_1 \vec{r}_2^*),$$

where  $\lambda_1 = \frac{x_3 x_3^* x_2}{x_3^2 - 1} - x_2^*$  and  $\lambda_2 = -\frac{x_3 x_3^* x_1}{x_3^2 - 1} + x_1^*$ . The dual vector  $\vec{D} = \vec{d} + \varepsilon \vec{d}^* = \oint \vec{\Psi}$  for  $\vec{\Psi} = \Psi_3 \vec{R}_3$ ,  $\Psi_3 = \frac{\Psi_3}{\Psi_3} + \varepsilon \Psi_3^*$  is the Steiner vector, where  $\vec{d} = (\oint \Psi_3) \vec{r}_3$  and  $\vec{d}^* =$

$(\phi \psi_3^*) \vec{r}_3 + (\phi \psi_3) \vec{r}_3^*$ . Consequently, the angle of pitch is vanishing, i.e.,

$$\lambda_T = \langle \vec{d}, \vec{t} \rangle = \left\langle \left( (\phi \psi_3) \vec{r}_3, \frac{1}{\sqrt{1-x_3^2}} (-x_2 \vec{r}_1 + x_1 \vec{r}_2) \right) \right\rangle = 0,$$

and the pitch is defined as

$$l_T = \langle \vec{d}^*, \vec{t} \rangle + \langle \vec{d}, \vec{t}^* \rangle.$$

From the equations

$$\begin{aligned} \langle \vec{d}, \vec{t}^* \rangle &= \left\langle \left( (\phi \psi_3) \vec{r}_3, \frac{1}{\sqrt{1-x_3^2}} (\lambda_1 \vec{r}_1 + \lambda_2 \vec{r}_2 - x_2 \vec{r}_1^* + x_1 \vec{r}_2^*) \right) \right\rangle \\ &= -\frac{1}{\sqrt{1-x_3^2}} \left( (\phi \psi_3) x_2 \langle \vec{r}_3, \vec{r}_1^* \rangle \right) \\ &\quad + \frac{1}{\sqrt{1-x_3^2}} \left( (\phi \psi_3) x_1 \langle \vec{r}_3, \vec{r}_2^* \rangle \right) \end{aligned}$$

and

$$\begin{aligned} \langle \vec{d}^*, \vec{t} \rangle &= \left\langle \left( (\phi \psi_3^*) \vec{r}_3 + (\phi \psi_3) \vec{r}_3^*, \frac{1}{\sqrt{1-x_3^2}} (-x_2 \vec{r}_1 + x_1 \vec{r}_2) \right) \right\rangle \\ &= -\frac{1}{\sqrt{1-x_3^2}} \left( (\phi \psi_3) x_2 \langle \vec{r}_3, \vec{r}_1 \rangle \right) \\ &\quad + \frac{1}{\sqrt{1-x_3^2}} \left( (\phi \psi_3) x_1 \langle \vec{r}_3, \vec{r}_2 \rangle \right), \end{aligned}$$

and since we have

$$\langle \vec{r}_3, \vec{r}_1^* \rangle = -\langle \vec{r}_3^*, \vec{r}_1 \rangle$$

and

$$\langle \vec{r}_3, \vec{r}_2^* \rangle = -\langle \vec{r}_3^*, \vec{r}_2 \rangle,$$

the pitch is

$$l_T = 0.$$

The dual angle of pitch is

$$\Lambda_T = l_T - \epsilon \lambda_T = 0.$$

Hence  $(T)$  is an extendable ruled surface.

**Theorem 7.** *The pitch, the angle of pitch, and the dual angle of pitch of the closed ruled surface  $(N)$  on the canonical coordinate frame are vanishing.*

*Proof.* We know that

$$\vec{N} = \frac{-1}{\sqrt{1-X_3^2}} (X_1 \vec{R}_1 + X_2 \vec{R}_2)$$

is valid, where  $\vec{N} = \vec{n} + \epsilon n^*$  and  $X_i = \vec{x}_i + \epsilon x_i^*$ ,  $\vec{R}_i = \vec{r}_i + \epsilon r_i^*$ ,  $i = 1, 2, 3$ , and

$$\begin{aligned} \vec{n} &= \frac{1}{\sqrt{1-x_3^2}} (x_1 \vec{r}_1 + x_2 \vec{r}_2), \\ \vec{n}^* &= \frac{1}{\sqrt{1-x_3^2}} \left( \left( x_1^* - \frac{x_3 x_3^* x_1}{x_3^2 - 1} \right) \vec{r}_1 \right. \\ &\quad \left. + \left( x_2 - \frac{x_3 x_3^* x_2}{x_3^2 - 1} \right) \vec{r}_2 + x_1 \vec{r}_1^* + x_2 \vec{r}_2^* \right). \end{aligned}$$

Since the Steiner vector is defined as  $\vec{D} = \vec{d} + \epsilon d^* = \phi \vec{\Psi}$  for  $\vec{\Psi} = \Psi_3 \vec{R}_3$ ,  $\Psi_3 = \psi_3 + \epsilon \psi_3^*$ , where  $\vec{d} = (\phi \psi_3) \vec{r}_3$  and  $\vec{d}^* = (\phi \psi_3^*) \vec{r}_3 + (\phi \psi_3) \vec{r}_3^*$ , the angle of pitch is vanishing, i.e.,

$$\begin{aligned} \lambda_N &= \langle \vec{d}, \vec{n} \rangle = \left\langle \left( (\phi \psi_3) \vec{r}_3, \frac{-1}{\sqrt{1-x_3^2}} (x_1 \vec{r}_1 + x_2 \vec{r}_2) \right) \right\rangle = 0, \end{aligned}$$

and the pitch is defined as

$$l_N = \langle \vec{d}^*, \vec{n} \rangle + \langle \vec{d}, \vec{n}^* \rangle.$$

From the equations

$$\begin{aligned} \langle \vec{d}, \vec{n}^* \rangle &= \left\langle \left( (\phi \psi_3) \vec{r}_3, \frac{-1}{\sqrt{1-x_3^2}} \left( \left( x_1^* - \frac{x_3 x_3^* x_1}{x_3^2 - 1} \right) \vec{r}_1 \right. \right. \right. \\ &\quad \left. \left. + \left( x_2 - \frac{x_3 x_3^* x_2}{x_3^2 - 1} \right) \vec{r}_2 + x_1 \vec{r}_1^* + x_2 \vec{r}_2^* \right) \right) \right\rangle \\ &= \frac{-x_1}{\sqrt{1-x_3^2}} \left( (\phi \psi_3) \langle \vec{r}_3, \vec{r}_1^* \rangle \right) \\ &\quad - \frac{x_2}{\sqrt{1-x_3^2}} \left( (\phi \psi_3) \langle \vec{r}_3, \vec{r}_2^* \rangle \right) \end{aligned}$$

and

$$\begin{aligned} \langle \vec{d}^*, \vec{n} \rangle &= \left\langle \left( (\phi \psi_3^*) \vec{r}_3 + (\phi \psi_3) \vec{r}_3^*, \frac{-1}{\sqrt{1-x_3^2}} (x_1 \vec{r}_1 + x_2 \vec{r}_2) \right) \right\rangle \\ &= \frac{-x_1}{\sqrt{1-x_3^2}} \left( (\phi \psi_3) \langle \vec{r}_3^*, \vec{r}_1 \rangle \right) \end{aligned}$$

$$-\frac{x_2}{\sqrt{1-x_3^2}} \left( \oint \psi_3 \right) \langle \vec{r}_3^*, \vec{r}_2 \rangle,$$

and since we have

$$\langle \vec{r}_3^*, \vec{r}_1^* \rangle = -\langle \vec{r}_3^*, \vec{r}_1 \rangle$$

and

$$\langle \vec{r}_3^*, \vec{r}_2 \rangle = -\langle \vec{r}_3^*, \vec{r}_2 \rangle,$$

the pitch is

$$l_N = 0.$$

The dual angle of pitch is

$$\Lambda_N = l_N - \varepsilon \lambda_N = 0.$$

So  $(N)$  is an extendable ruled surface.

**Theorem 8.** *The pitch, the angle of pitch, and the dual angle of pitch of the closed ruled surface  $(B)$  on the canonical coordinate frame are vanishing.*

*Proof.* This is clear since we have  $B = \mathbb{R}^3$ , so this ruled surface is extendable.

**Theorem 9.** *The pitch, the angle of pitch, and the dual angle of pitch of the closed ruled surface  $(D_0)$  on the canonical coordinate frame are given by*

$$l_{D_0} = \frac{1}{\sqrt{k_1^2 + k_2^2}} \left[ k_1^* \left( \oint \psi_3 \right) + k_1 \left( \oint \psi_3^* \right) \right],$$

$$\lambda_{D_0} = \frac{k_1}{\sqrt{k_1^2 + k_2^2}} \left( \oint \psi_3 \right),$$

and

$$\Lambda_{D_0} = \frac{1}{\sqrt{k_1^2 + k_2^2}} \left[ k_1^* \left( \oint \psi_3 \right) + k_1 \left( \oint \psi_3^* \right) \right]$$

$$- \varepsilon \frac{k_1}{\sqrt{k_1^2 + k_2^2}} \left( \oint \psi_3 \right),$$

respectively.

*Proof.* We know that

$$\vec{D}_0 = \frac{\tau \vec{T} + \kappa \vec{B}}{\sqrt{\tau^2 + \kappa^2}}$$

$$= \frac{1}{\sqrt{\tau^2 + \kappa^2}} \left[ \frac{\tau}{\sqrt{1-X_3^2}} \left( -X_2 \vec{R}_1 + X_1 \vec{R}_2 \right) + \kappa \vec{R}_3 \right]$$

is valid, where  $\vec{D}_0 = \vec{d} + \varepsilon d^*$ ,  $\kappa = k_1 + \varepsilon k_1^*$ ,  $\tau = k_2 + \varepsilon k_2^*$ ,  $X_i = \vec{x}_i + \varepsilon x_i^*$  and  $\vec{R}_i = \vec{r}_i + \varepsilon r_i^*$  for  $i = 1, 2, 3$ . We have

$$\vec{d}_0 = \frac{1}{\sqrt{k_1^2 + k_2^2}} \left[ \frac{k_2}{\sqrt{1-x_3^2}} \left( -x_2 \vec{r}_1 + x_1 \vec{r}_2 \right) + k_1 \vec{r}_3 \right],$$

$$\vec{d}_0^* = \frac{1}{\sqrt{k_1^2 + k_2^2}} \left( -x_2^* \vec{r}_1 + k_2 x_1^* \vec{r}_2 - k_2 x_2 \vec{r}_1^* \right.$$

$$\left. + k_2 x_1 \vec{r}_2^* + k_1 \vec{r}_3^* + k_1^* \vec{r}_3 \right.$$

$$\left. - \left( k_2 \frac{k_2^* k_2 + k_1^* k_1}{k_1^2 + k_2^2} + k_2 \frac{x_3 x_3^*}{x_3^2 - 1} + k_2^* \right) \left( x_2 \vec{r}_1 + x_1 \vec{r}_2 \right) \right).$$

From the definition of the Steiner vector, the angle of pitch is

$$\lambda_{D_0} = \langle \vec{d}, \vec{d}_0 \rangle$$

$$= \left\langle \left( \oint \psi_3 \right) \vec{r}_3, \right.$$

$$\left. \frac{1}{\sqrt{k_1^2 + k_2^2}} \left( \frac{k_2}{\sqrt{1-x_3^2}} \left( -x_2 \vec{r}_1 + x_1 \vec{r}_2 \right) + k_1 \vec{r}_3 \right) \right\rangle$$

$$= \frac{k_1}{\sqrt{k_1^2 + k_2^2}} \oint \psi_3,$$

and the pitch of  $(D_0)$  is given by

$$l_{D_0} = \langle \vec{d}^*, \vec{d}_0 \rangle + \langle \vec{d}, \vec{d}_0^* \rangle.$$

From

$$\langle \vec{d}, \vec{d}_0^* \rangle = \frac{1}{\sqrt{k_1^2 + k_2^2}} \left[ \frac{-k_2 x_2}{\sqrt{1-x_3^2}} \left( \oint \psi_3 \right) \langle \vec{r}_3, \vec{r}_1^* \rangle \right.$$

$$\left. + \frac{k_2 x_1}{\sqrt{1-x_3^2}} \left( \oint \psi_3 \right) \langle \vec{r}_3, \vec{r}_2^* \rangle + k_1^* \left( \oint \psi_3 \right) \right]$$

and

$$\langle \vec{d}^*, \vec{d}_0 \rangle = \left\langle \left( \oint \psi_3^* \right) \vec{r}_3 + \left( \oint \psi_3 \right) \vec{r}_3^*, \right.$$

$$\left. \frac{1}{\sqrt{k_1^2 + k_2^2}} \left[ \frac{k_2}{\sqrt{1-x_3^2}} \left( -x_2 \vec{r}_1 + x_1 \vec{r}_2 \right) + k_1 \vec{r}_3 \right] \right\rangle$$

$$= \frac{1}{\sqrt{k_1^2 + k_2^2}} \left[ \frac{-k_2 x_2}{\sqrt{1-x_3^2}} \left( \oint \psi_3 \right) \langle \vec{r}_3^*, \vec{r}_1 \rangle \right.$$

$$\left. + \frac{k_2 x_1}{\sqrt{1-x_3^2}} \left( \oint \psi_3 \right) \langle \vec{r}_3^*, \vec{r}_2 \rangle + k_1 \left( \oint \psi_3^* \right) \right]$$

and since we have

$$\langle \vec{r}_3, \vec{r}_1^* \rangle = -\langle \vec{r}_3^*, \vec{r}_1 \rangle$$

and

$$\langle \vec{r}_3, \vec{r}_2^* \rangle = -\langle \vec{r}_3^*, \vec{r}_2 \rangle,$$

the pitch is

$$l_{D_0} = \frac{1}{\sqrt{k_2^2 + k_1^2}} \left[ k_1^* \left( \oint \psi_3 \right) + k_1 \left( \oint \psi_3^* \right) \right].$$

The dual angle of pitch of  $(D_0)$  is

$$\begin{aligned} \Lambda_{D_0} &= l_{D_0} - \varepsilon \lambda_{D_0} \\ &= \frac{1}{\sqrt{k_1^2 + k_2^2}} \left[ k_1^* \left( \oint \psi_3 \right) + k_1 \left( \oint \psi_3^* \right) \right] \\ &\quad - \varepsilon \frac{k_1}{\sqrt{k_1^2 + k_2^2}} \left( \oint \psi_3 \right). \end{aligned}$$

This completes the proof.

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